# PRODUCT APPROVAL SUPPORTING CALCULATIONS Premium Vinyl Tilt Double Hung Window

REPORT TO:

JELD-WEN WINDOWS & DOORS 3737 LAKEPORT BLVD KLAMATH FALLS, OREGON

REPORT NUMBER: NCTL-110-24718-1 REPORT DATE: 10/27/21

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## **Scope**

National Certified Testing Laboratories was contracted by Jeld-Wen Windows & Doors to evaluate alternate installation methods for their *Premium Vinyl* Tilt Double Hung Window. The evaluation is based on physical testing and product certifications. Reference standards utilized in this project include:

Florida Building Code, Building. International Code Council.

ANSI/AWC *National Design Specification (NDS) for Wood Construction*. American Wood Council.

AISI S100 North American Specification for the Design of Cold-Formed Steel Structural Members. American Iron and Steel Institute.

ICC-ES Report ESR-1976 *ITW Buildex TEKS Self-Drilling Fasteners*. ICC Evaluation Service.

NOA 21-0201.06 Tapcon Concrete and Masonry Anchors with Advanced Threadform Technology. Miami-Dade County Product Control Section.

The anchorage analyses presented herein do not address the water resistance, water penetration or air infiltration performance of the installation method or the installed product. In addition, the analyses rely on the assumption that the building substrate is capable of withstanding incurred loads.

#### Certification of Independence

In accordance with Rule 61G20-3 Florida Administrative Code, National Certified Testing Laboratories hereby certifies the following:

- National Certified Testing Laboratories does not have, nor does it intend to acquire
  or will it acquire, a financial interest in any company manufacturing or distributing
  products tested or labeled by the agency.
- National Certified Testing Laboratories is not owned, operated or controlled by any company manufacturing or distributing products it tests or labels.
- Joseph A. Reed, P.E. does not have nor will acquire, a financial interest in any company manufacturing or distributing products for which the reports are being issued.
- Joseph A. Reed, P.E does not have, nor will acquire, a financial interest in any other entity involved in the approval process of the product.



#### **Analyses**

## **Summary of Test Results**

The following table summarizes the various *Premium Vinyl* Tilt Double Hung Window products and their corresponding performance levels which have been established by testing or product certification.

**Table 1** Summary of Test Results

Series/Model	Test Report Number	Size (W x H)	Performance
Premium Vinyl Tilt Double Hung (Fin Install and Frame Install)	ESP024843P.6 (Rev. 1, 05/16/17)	48" x 77"	+50/-55 psf
Premium Vinyl Tilt Double Hung, XOX (Fin Install and Strap Install)	H0700.15-3047 (Rev, 06/09/17)	108" x 72"	+50/-55 psf
Premium Vinyl Tilt Double Hung, XOX (Fin Install and Strap Install)	ESP026028P.1 (Rev, 08/08/17)	120" x 84"	+35/-40 psf

Testing documented in Table 1 was conducted the Element Testing laboratory in Wausau, Wisconsin (Florida Department of Business & Professional Regulation Test Lab No. TST2613, A2LA Certificate 1479.01) and the Intertek laboratory in Fresno, California (Florida Department of Business & Professional Regulation Test Lab No. TST2609, IAS Laboratory Accreditation TL-264).

#### **As-Tested Installation Analysis**

For air/water/structural testing the test specimen was secured to a 2x Spruce-Pine-Fir buck. The as-tested installation methods are evaluated on page 4 to page 10. These capacities will be used to prove acceptable alternate anchors and substrates for the windows.

#### **Alternate Anchorages**

Calculations on page 11 through page 19 determine the design capacity of alternate installation anchorages for the window.

## **Anchorage Requirements**

As-tested spacing must be maintained. It must be determined the anchorages are not overloaded for the approved window size and design pressures. Calculations presented on page 20 and page 21 show the anchor spacing requirements for the established limiting anchor capacities.

Anchorage requirements established by this report are accurately presented in Drawing D014484 and Drawing D014539.



## **Attachments**

Appendix A – Revision Log (1 page)



## **As-Tested Installation – Nail Fin to Wood**

#8 x 1-1/4" Pan Head Screw

0.062" thick Nail Fin

Spruce-Pine-Fir 2x Wood Substrate Minimum (G=0.42)

## Allowable Tension of #8 x 1-1/4" Pan Head Screw

W = 1.6(1.250"-0.062")(82 lb/in) (NDS, Table 11.2B)

W = 156 lb

## Allowable Pull-Over of #8 x 1-1/4" Pan Head Screw

Validated by Testing

As-tested spacing: 12" on center

As-tested Window Width: 48" As-tested Pressure: 55 psf

As-tested Anchor Load: (48"/2)(12")(55 psf/144) = 110 lb/anchor

**Capacity of Connection is 110 lb** 



## <u>As-Tested Installation – Through Frame to Wood</u>

#8 Pan Head Screw; 1-1/2" penetration to wood

0.062" thick Window Frame

1/4" Maximum Shim Space

Spruce-Pine-Fir 2x Wood Substrate Minimum (G=0.42)

## Allowable Shear of #8 Pan Head Screw

Z' = 113 lb (See Following 2 Pages)

#### Bending of #8 Pan Head Screw

L = 1/4" (maximum shim space)

 $S = \pi d^3/32 = \pi (0.131)^3/32 = 0.000221 in^3$ 

 $F_b = (1.3)(0.6F_y) = (1.3)(0.6)(90,000 \text{ psi}) = 70,200 \text{ psi} (1.3 \text{ weak axis factor})$ 

 $F_b = M/S = (VL/2)/S (L/2 \text{ for guided bending})$ 

 $V = 2SF_b/L = (2)(0.000221 in)(70,200 psi)/0.25" = 124 lb.$ 

**Capacity of Connection is 113 lb** 



# <u>As-Tested Installation – Through Frame to Wood</u> (Continued)

## **Lateral Design Strength of Wood Connections**

#### Data

Fastener			
Fastener	=	#8 W	ood Screw
Shank Dia	=	0.164	in.
Root Dia.	=	0.131	in.
$F_{yb}$	=	90,000	psi
Fastener length	=	2.500	in.

#### **Main Member**

Material	=		SPF	
G	=	0.42		
θ	=	90	<= (Angle of loa	d to grain $0^{\circ} \le \theta \le 90^{\circ}$ )
$F_{e}$	=	3,350	psi	
Thickness	=	1.500	in.	

#### Side Member

Material	=	Vin	yl (PVC)	
G	=	N/A		
θ	=	90	<= (Angle of load	d to grain $0^{\circ} \le \theta \le 90^{\circ}$ )
$F_{es}$	=	13,750	psi	
Thickness	=	0.125	in.	

#### **Calculations**

#### **Lateral Bearing Factors**

D	=	0.131	in
$\ell_{\rm m}$	=	1.500	in
$K_{\boldsymbol{\theta}}$	=	1.25	
$K_D$	=	2.20	
$R_{e}$	=	0.244	
$R_{t}$	=	12.00	
$\mathbf{k}_1$	=	1.1349	
$k_2$	=	0.6403	
$k_3$	=	6.37	

Yield Mode	$R_{d}$
$I_{m}$ , $I_{s}$	2.20
II	2.20
III <sub>m</sub> , III <sub>s</sub> , IV	2.20



# <u>As-Tested Installation – Through Frame to Wood</u> (Continued)

Lateral Des	ign Valu	ıes, Z		
$Mode I_m$	=	299	lbf	
Mode I <sub>s</sub>	=	102	lbf	
Mode II	=	116	lbf	
$Mode\ III_{m}$	=	129	lbf	
Mode III <sub>s</sub>	=	71	lbf	<===== Minimum Value
Mode IV	=	99	lbf	
$C_{\scriptscriptstyle D}$	=	1.6		
		ice Factor		
Fabrication/In-	Service	Dry/Dry		
$C_{M}$	=	1.0		
In service temp	erature	T:	≤100°F	
$C_{t}$	=	1.0		
$C_g$	=	1.0		
$C_{\!\scriptscriptstyle \Delta}$	=	1.0		
Is fastener installed in end	grain?	No		
$C_{eg}$	=	1.00		
Is fastener part of a diap	hragm?	No		
$C_{di}$	=	1.0		
Is fastener toe-	nailed?	No		
$C_{tn}$	=	1.00		
Z'	=	<u>113</u>	lbf	



## As-Tested Installation - Strap Anchor to Wood

Two #8 x 1-1/2" Pan Head Screws securing strap to substrate

Spruce-Pine-Fir 2x Wood Substrate Minimum (G=0.42)

Two #8 Screws securing strap to window frame

0.125" thick Window Frame

20 gauge (0.033" thick) 33 KSI Steel Strap Anchor

1/4" Maximum Shim Space

#### Allowable Shear of #8 x 1-1/2" Pan Head Screw

Z' = 122 lb (See Following 2 Pages)

## Bending of #8 x 1-1/2" Pan Head Screw

L = 1/4" (maximum shim space)

 $S = \pi d^3/32 = \pi (0.131)^3/32 = 0.000221 \text{ in}^3$ 

 $F_b = (1.3)(0.6F_v) = (1.3)(0.6)(90,000 \text{ psi}) = 70,200 \text{ psi} (1.3 \text{ weak axis factor})$ 

 $F_b = M/S = (VL/2)/S (L/2 \text{ for guided bending})$ 

 $V = 2SF_b/L = (2)(0.000221 \text{ in})(70,200 \text{ psi})/0.25" = 124 \text{ lb.}$ 

#### Bearing of #8 Screw on Frame

 $F_p = 10,000 \text{ psi}$ 

D = 0.164"

t = 0.125"

 $V_a = F_pDt = (10,000 \text{ psi})(0.164")(0.125") = 205 \text{ lb}$ 

#### Bearing of #8 Screw on Strap Anchor

 $V_a = 2.7 Dt F_{tu}/3.0$ 

 $V_a = 2.7(0.164")(0.033")(45,000 psi)/3.0$ 

 $V_a = 219 \text{ lb.}$ 

**Capacity of Connection is 122 lb** 

Capacity for Two Screws is 244 lb

Qualifies 8d (0.131" diameter) Nail

**Fastener** 



# As-Tested Installation - Strap Anchor to Wood (Continued)

## **Lateral Design Strength of Wood Connections**

#### Data

Fastener	=	#8 W	ood Screw
Shank Dia	=	0.164	in.
Root Dia.	=	0.131	in.
$F_{yb}$	=	90,000	psi
Fastener length	=	2.500	in.
Main Memb	er		
Material	=		SPF
G	=	0.42	
θ	=	90	$<=$ (Angle of load to grain $0^{\circ} < \theta < 90^{\circ}$ )
$F_{e}$	=	3,350	psi
Thickness	=	1.500	in.

#### **Side Member**

Material	=	ASTM A 653	<mark>3, Grade 33 Steel</mark>
G	=	N/A	
θ	=	90	$<=$ (Angle of load to grain $0^{\circ} < \theta < 90^{\circ}$ )
$F_{es}$	=	61,850	psi
Thickness	=	0.033	in.

#### **Calculations**

## Lateral Bearing Factors

D	=	0.131	in
$\ell_{\rm m}$	=	1.500	in
$K_{\boldsymbol{\theta}}$	=	1.25	
$K_D$	=	2.20	
$R_{e}$	=	0.054	
$R_{t}$	=	45.45	
$\mathbf{k}_1$	=	1.0041	
$k_2$	=	0.5032	
$k_3$	=	23.87	

Yield Mode	$R_d$
$I_{\rm m}$ , $I_{\rm s}$	2.20
II	2.20
III <sub>m</sub> , III <sub>s</sub> , IV	2.20



# As-tested Installation - Strap Anchor to Wood (Continued)

Lateral Desi	gn Valu	ies, Z		
$Mode\ I_{m}$	=	299	lbf	
Mode I <sub>s</sub>	=	122	lbf	
Mode II	=	122	lbf	
Mode III <sub>m</sub>	=	136	lbf	
Mode III <sub>s</sub>	=	77	lbf	<===== Minimum Value
Mode IV	=	108	lbf	
$C_{\mathtt{D}}$	=	1.6		
V	Jet Serv	ice Factor		
Fabrication/In-	Service	Dry/Dry		
$C_M$	=	1.0		
In service tempo	erature	T:	≤100°F	
$C_{t}$	=	1.0		
$C_g$	=	1.0		
$C_{\Delta}$	=	1.0		
Is fastener installed in end	grain?	No		
$C_{eg}$	=	1.00		
Is fastener part of a diapl	nragm?	No		
$C_{d\mathrm{i}}$	=	1.0		
Is fastener toe-	nailed?	No		
$C_{tn}$	=	1.00		
Z'	=	<u>122</u>	lbf	



## <u>Alternate Installation - Trough Frame to Steel Stud</u>

#10-16 TEKS Screw

1/4" Maximum Shim Space

Minimum 18 gauge 33 KSI Steel Stud

#### Allowable Shear of #10-16 TEKS Screw

 $P_{ss}/\Omega = 573 \text{ lb (ESR-1976)}$ 

#### Bearing of #10-16 TEKS Screw on Frame

 $F_p = 10,000 \text{ psi}$  D = 0.190" t = 0.125"  $V_a = F_pDt = (10,000 \text{ psi})(0.190)(0.125) = 238 \text{ lb}$ 

## Bearing of #10-16 TEKS Screw on Steel Stud

 $V_a = 2.7 DtF_{tu}/3.0$   $V_a = 2.7(0.190")(0.0428")(45,000 psi)/3.0$  $V_a = 329 lb.$ 

#### Tilting of #10-16 TEKS Screw in Steel Stud

 $V_a = 4.2(t_2{}^3D)^{1/2}F_{tu2}/n_s$   $V_a = 4.2(0.0428"^3 \text{ x } 0.190")^{1/2}(45,000 \text{ psi})/3.0$   $V_a = 243 \text{ lb.}$ 

#### Bending of #10-16 TEKS Screw

 $L = 1/4" \text{ (Maximum Shim Space)} \\ S = \pi d^3/32 = \pi (0.135)^3/32 = 0.000242 \text{ in}^3 \\ F_b = (1.3)(0.6F_y) = (1.3)(0.6)(92,000 \text{ psi}) = 71,760 \text{ psi} (1.3 \text{ weak axis factor}) \\ F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)} \\ V = 2SF_b/L = (2)(0.000242 \text{ in}^3)(71,760 \text{ psi})/0.25" = 139 \text{ lb.} \\ \end{split}$ 

#### Capacity of Connection is 139 lb.



## Alternate Installation – Through Frame to Concrete

3/16" Tapcon Anchor

2-1/2" Minimum Edge Distance, 1-1/4" Minimum Embedment

1/4" Maximum Shim Space

Minimum f'c = 3,000 psi Concrete

#### Allowable Shear of 3/16" Tapcon Anchor

 $P_{ss}/\Omega = 181 \text{ lb}$  (NOA-No. 16-1222.06)

## Bearing of 3/16" Tapcon Anchor on Frame

 $F_p = 10,000 \text{ psi}$  D = 0.170" t = 0.125"  $V_a = F_pDt = (10,000 \text{ psi})(0.170)(0.125) = 213 \text{ lb}$ 

## Bending of 3/16" Tapcon Anchor

 $L = 1/4" \text{ (Maximum Shim Space)} \\ S = \pi d^3/32 = \pi (0.170")^3/32 = 0.000482 \text{ in}^3 \\ F_b = (1.3)(0.6F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} (1.3 \text{ weak axis factor}) \\ F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)} \\ V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb.} \\$ 

**Capacity of Connection is 181 lb** 



## <u>Alternate Installation – Through Frame to CMU</u>

3/16" Tapcon Anchor

2-1/2" Minimum Edge Distance, 1-1/4" Minimum Embedment

1/4" Maximum Shim Space

Minimum ASTM C90 Concrete Masonry Unit

## Allowable Shear of 3/16" Tapcon Anchor

 $P_{ss}/\Omega = 135 \text{ lb}$  (NOA-No. 16-1222.06)

## Bearing of 3/16" Tapcon Anchor on Frame

 $F_p = 10,000 \text{ psi}$  D = 0.170" t = 0.125"  $V_a = F_pDt = (10,000 \text{ psi})(0.170)(0.125) = 213 \text{ lb}$ 

## Bending of 3/16" Tapcon Anchor

 $L = 1/4" \text{ (Maximum Shim Space)} \\ S = \pi d^3/32 = \pi (0.170")^3/32 = 0.000482 \text{ in}^3 \\ F_b = (1.3)(0.6F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} (1.3 \text{ for weak axis bending)} \\ F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)} \\ V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb.} \\ \end{split}$ 

**Capacity of Connection is 135 lb** 



## Alternate Installation - Strap Anchor to Concrete

3/16" Tapcon Anchor; 2-1/2" Minimum Edge Distance, 1-1/4" Minimum Embedment

#8 Screws Connecting Strap to Window Frame

0.125" thick Window Frame

20 gauge (0.033" thick) 33 KSI Steel Strap Anchor

1/4" Maximum Shim Space

Minimum f'c = 3,000 psi Concrete

## Allowable Shear of 3/16" Tapcon Anchor

 $P_{ss}/\Omega = 181 \text{ lb}$  (NOA-No. 16-1222.06)

## Bearing of 3/16" Tapcon Anchor on Strap Anchor

 $V_a = 2.7 Dt F_{tu}/3.0$ 

 $V_a = 2.7(0.170")(0.033")(45,000 psi)/3.0$ 

 $V_a = 227 \text{ lb.}$ 

#### Bending of 3/16" Tapcon Anchor

L = 1/4" (Maximum Shim Space)

 $S = \pi d^3/32 = \pi (0.170'')^3/32 = 0.000482 in^3$ 

 $F_b = (1.3)(0.6F_v) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} (1.3 \text{ weak axis factor})$ 

 $F_b = M/S = (VL/2)/S (L/2 \text{ for guided bending})$ 

 $V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb}.$ 

#### Bearing of #8 Screw on Strap Anchor

 $V_a = 2.7 Dt F_{tu}/3.0$ 

 $V_a = 2.7(0.164")(0.033")(45,000 psi)/3.0$ 

 $V_a = 219 \text{ lb.}$ 



## <u>Alternate Installation – Strap Anchor to Concrete</u> (Continued)

## Bearing of #8 Screw on Frame

 $F_p$  = 10,000 psi D = 0.164" t = 0.125"  $V_a = F_p Dt = (10,000 \text{ psi})(0.164")(0.125") = 205 \text{ lb}$ 

**Capacity of Connection is 181 lb** 



## Alternate Installation - Strap Anchor to CMU

3/16" Tapcon Anchor; 2-1/2" Minimum Edge Distance, 1-1/4" Minimum Embedment

#8 Screws Connecting Strap to Window Frame

0.125" thick Window Frame

20 gauge (0.033" thick) 33 KSI Steel Strap Anchor

1/4" Maximum Shim Space

Minimum ASTM C90 Concrete Masonry Unit

## Allowable Shear of 3/16" Tapcon Anchor

 $P_{ss}/\Omega = 135 \text{ lb}$  (NOA-No. 16-1222.06)

## Bearing of 3/16" Tapcon Anchor on Strap Anchor

 $V_a = 2.7 Dt F_{tu}/3.0$ 

 $V_a = 2.7(0.170")(0.033")(45,000 psi)/3.0$ 

 $V_a = 227 \text{ lb.}$ 

#### Bending of 3/16" Tapcon Anchor

L = 1/4" (Maximum Shim Space)

 $S = \pi d^3/32 = \pi (0.170'')^3/32 = 0.000482 in^3$ 

 $F_b = (1.3)(0.6F_v) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} (1.3 \text{ for weak axis bending})$ 

 $F_b = M/S = (VL/2)/S (L/2 \text{ for guided bending})$ 

 $V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb}.$ 

#### Bearing of #8 Screw on Strap Anchor

 $V_a = 2.7 Dt F_{tu}/3.0$ 

 $V_a = 2.7(0.164")(0.033")(45,000 psi)/3.0$ 

 $V_a = 219 \text{ lb.}$ 



# <u>Alternate Installation – Strap Anchor to CMU</u> (Continued)

## Bearing of #8 Screw on Frame

 $F_p$  = 10,000 psi D = 0.164" t = 0.125"  $V_a$  =  $F_p$ Dt = (10,000 psi)(0.164")(0.125") = 205 lb

**Capacity of Connection is 135 lb** 



## Alternate Installation - Strap Anchor to Steel Stud

#10-16 TEKS Screws Connecting Strap to Steel Stud

#8 Screws Connecting Strap to Window Frame

0.125" thick Window Frame

18 gauge (0.043" thick) 33 KSI Steel Stud

20 gauge (0.033" thick) 33 KSI Steel Strap Anchor

1/4" Maximum Shim Space

## Allowable Shear of #10-16 TEKS Screw

 $P_{ss}/\Omega = 573 \text{ lb (ESR-1976)}$ 

## Bearing of #10-16 TEKS Screw on Steel Strap Anchor

 $V_a = 2.7 Dt F_{tu}/3.0$ 

 $V_a = 2.7(0.190")(0.033")(45,000 psi)/3.0$ 

 $V_a = 253 \text{ lb.}$ 

#### Bearing of #10-16 TEKS Screw on Steel Stud

 $V_a = 2.7 Dt F_{tu}/3.0$ 

 $V_a = 2.7(0.190")(0.043")(45,000 psi)/3.0$ 

 $V_a = 331 \text{ lb.}$ 

#### Tilting of #10-16 TEKS Screw in Steel Stud

 $V_a = 4.2(t_2^3D)^{1/2}F_{tu2}/n_s$ 

 $V_a = 4.2(0.0428^{\circ 3} \times 0.190^{\circ})^{1/2}(45,000 \text{ psi})/3.0$ 

 $V_a = 243 \text{ lb.}$ 

## Bending of #10-16 TEKS Screw

L = 1/4" (Maximum Shim Space)

 $S = \pi d^3/32 = \pi (0.135)^3/32 = 0.000242 \text{ in}^3$ 

 $F_b = (1.3)(0.6F_v) = (1.3)(0.6)(92,000 \text{ psi}) = 71,760 \text{ psi} (1.3 \text{ weak axis factor})$ 

 $F_b = M/S = (VL/2)/S (L/2 \text{ for guided bending})$ 

 $V = 2SF_b/L = (2)(0.000242 \text{ in}^3)(71.760 \text{ psi})/0.25" = 139 \text{ lb}.$ 



## <u>Alternate Installation – Strap Anchor to Steel Stud</u> (Continued)

## Bearing of #8 Screw on Strap Anchor

 $V_a = 2.7 \text{DtF}_{tu}/3.0$   $V_a = 2.7(0.164")(0.033")(45,000 \text{ psi})/3.0$  $V_a = 219 \text{ lb}.$ 

## Bearing of #8 Screw on Frame

$$\begin{split} F_p &= 10,000 \text{ psi} \\ D &= 0.164\text{"} \\ t &= 0.125\text{"} \\ V_a &= F_p D t = (10,000 \text{ psi})(0.164\text{"})(0.125\text{"}) = 205 \text{ lb} \end{split}$$

Capacity of Connection is 139 lb



## 48 x 77 +50/-55 psf

#### Anchorage Requirements - Nail Fin

Window Overall Size: 48" x 77"

Window Overall Area:  $(48")(77")/144 = 25.7 \text{ ft}^2$ Window Overall Wind Load:  $(55 \text{ psf})(25.7 \text{ ft}^2) = 1,414 \text{ lb}$ 

Installed Anchors: 4 head + 4 sill + 2(7) jambs = 22 installed anchors

Minimum Anchor Capacity: 110 lb/anchor

Total Anchor Capacity:  $(22 \text{ anchors})(110 \text{ lb/anchor}) = 2,420 \text{ lb} > 1,414 \text{ lb } \mathbf{OK}$ 

## **Anchorage Requirements – Through Frame**

Window Overall Size: 48" x 77"

Window Overall Area:  $(48")(77")/144 = 25.7 \text{ ft}^2$ Window Overall Wind Load:  $(55 \text{ psf})(25.7 \text{ ft}^2) = 1,414 \text{ lb}$ 

Installed Anchors: 3 head + 3 sill + 2(5) jambs = 16 installed anchors

Minimum Anchor Capacity: 113 lb/anchor

Total Anchor Capacity: (16 anchors)(113 lb/anchor) = 1,808 lb > 1,414 lb **OK** 

#### 120x 84 +35/-40 psf

#### Anchorage Requirements - Nail Fin

Window Overall Size: 120" x 84"

Window Overall Area:  $(120")(84")/144 = 70.0 \text{ ft}^2$ Window Overall Wind Load:  $(40 \text{ psf})(70.0 \text{ ft}^2) = 2,800 \text{ lb}$ 

Installed Anchors: 15 head + 15 sill + 2(10) jambs = 50 installed anchors

Minimum Anchor Capacity: 110 lb/anchor

Total Anchor Capacity: (50 anchors)(110 lb/anchor) = 5,500 lb > 2,800 lb

#### **Anchorage Requirements – Strap Anchor**

Window Overall Size: 120" x 84"

Window Overall Area:  $(120")(84")/144 = 70.0 \text{ ft}^2$ Window Overall Wind Load:  $(40 \text{ psf})(70.0 \text{ ft}^2) = 2,800 \text{ lb}$ 

Installed Anchors: 10 head + 10 sill + 2(5) jambs = 30 installed anchors

Minimum Anchor Capacity: 122 lb/anchor

Total Anchor Capacity: (30 anchors)(122 lb/anchor) = 3,660 lb > 2,800 lb **OK** 



## 108 x 72 +50/-55 psf

## Anchorage Requirements - Nail Fin

Window Overall Size: 108" x 72"

Window Overall Area:  $(108")(72")/144 = 54.0 \text{ ft}^2$ Window Overall Wind Load:  $(55 \text{ psf})(54.0 \text{ ft}^2) = 2,970 \text{ lb}$ 

Installed Anchors: 15 head + 15 sill + 2(5) jambs = 40 installed anchors

Minimum Anchor Capacity: 110 lb/anchor

Total Anchor Capacity: (40 anchors)(110 lb/anchor) = 4,400 lb > 2,970 lb

#### **Anchorage Requirements – Strap Anchor**

Window Overall Size: 108" x 72"

Window Overall Area:  $(108")(72")/144 = 54.0 \text{ ft}^2$ Window Overall Wind Load:  $(55 \text{ psf})(54.0 \text{ ft}^2) = 2,970 \text{ lb}$ 

Installed Anchors: 13 head + 13 sill + 2(5) jambs = 36 installed anchors

Minimum Anchor Capacity: 122 lb/anchor

Total Anchor Capacity: (36 anchors)(122 lb/anchor) = 4,392 lb > 2,970 lb **OK** 

## Anchorage Requirements – Through Frame

Window Overall Size: 108" x 72"

Window Overall Area:  $(108")(72")/144 = 54.0 \text{ ft}^2$ Window Overall Wind Load:  $(55 \text{ psf})(54.0 \text{ ft}^2) = 2,970 \text{ lb}$ 

Installed Anchors: 13 head + 13 sill + 2(5) jambs = 36 installed anchors

Minimum Anchor Capacity: 139 lb/anchor

Total Anchor Capacity: (36 anchors)(139 lb/anchor) = 5,004 lb > 2,970 lb **OK** 



# Appendix A

# Revision Log

<u>Identification</u> <u>Date</u> <u>Page & Revision</u>

Original Issue 10/27/21 Not Applicable